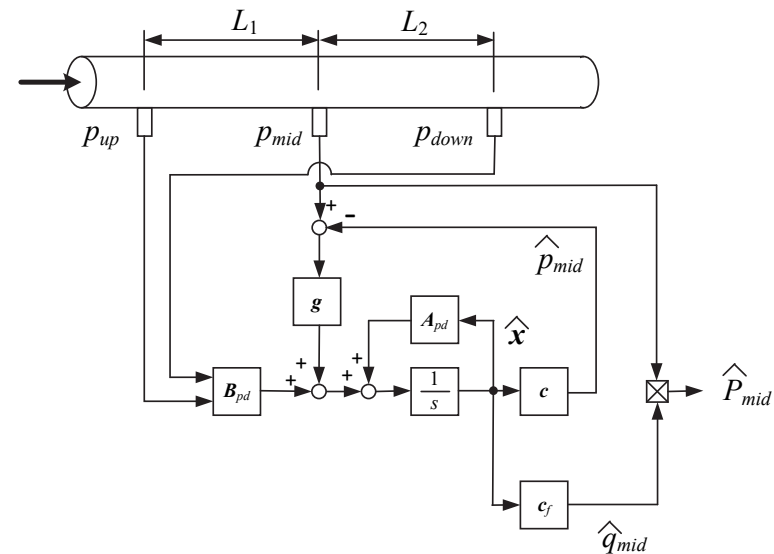


Condition for Real-time Measurement of Power of Unsteady Fluid Flow in a Pipe by Kalman Filter

Kazushi SANADA
Yokohama National
University, Japan



-
- 1 Introduction
 - 2 Kalman filter theory
 - 3 Plant model of Kalman filter: Pipeline dynamics model
 - 4 Off-line estimation of unsteady flow rate by Kalman filter
 - 5 Real-time implementation of Kalman filter
 - 6 Conclusion
-

1. Introduction

Electromagnetic flowmeter



http://www.keyence.co.jp/atsuryoku/ryuryou/fd_m/

Coriolis flow meter



http://www.keyence.co.jp/atsuryoku/ryuryou/fd_s/

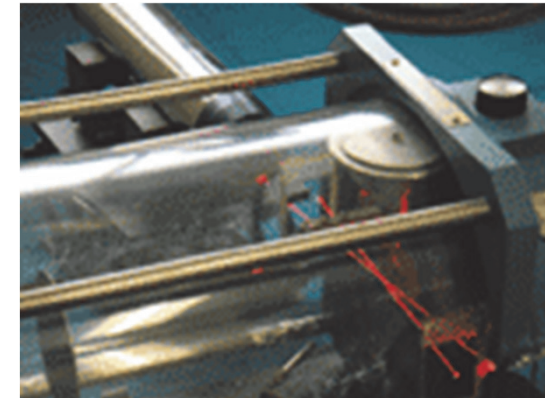
Ultrasonic flowmeter



http://www.fujielectric.co.jp/products/instruments/products/flow_ultra/FSV.html

Velocity distribution

Laser Doppler flow velocimeter



<http://www.kanomax.co.jp/fsmart.html>

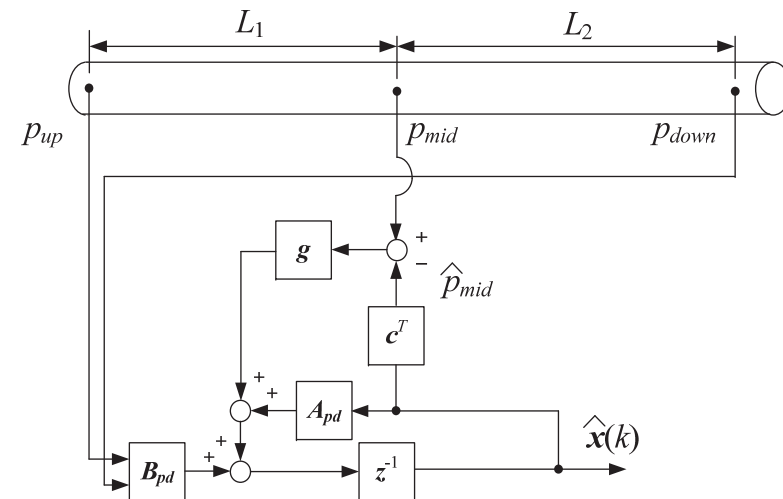
Pin-point Velocity

○ Direct measurement in real-time

- × sensor may disturb flow
- × sensor is influenced by velocity distribution
- × time-special distribution is not obtained

1. Introduction

- Kalman filter is proposed to estimate unsteady fluid flow in a pipe using a model of pipeline dynamics.
- The merit of this method is to use only three pressure sensors without flow sensor which may disturb flow in a pipe.
- The aim of this research is to develop a real-time indirect measurement system of unsteady flow rate and fluid power in a pipe.



2. Kalman filter theory

Kalman filter estimates the optimal state variables of a system which is disturbed by noise.

$$\mathbf{x}_p(k+1) = \mathbf{A}_{pd}\mathbf{x}_p(k) + \mathbf{B}_{pd}\bar{\mathbf{p}}(k) + \mathbf{B}_{pd}\mathbf{v}(k), \text{ and}$$

$$p_{mid}(k) = \mathbf{c}^T \mathbf{x}_p(k) + w(k).$$

Priori estimation $\hat{\mathbf{x}}^-(k) = \mathbf{A}_{pd}\hat{\mathbf{x}}(k-1) + \mathbf{B}_{pd}\bar{\mathbf{p}}(k-1), \text{ and}$

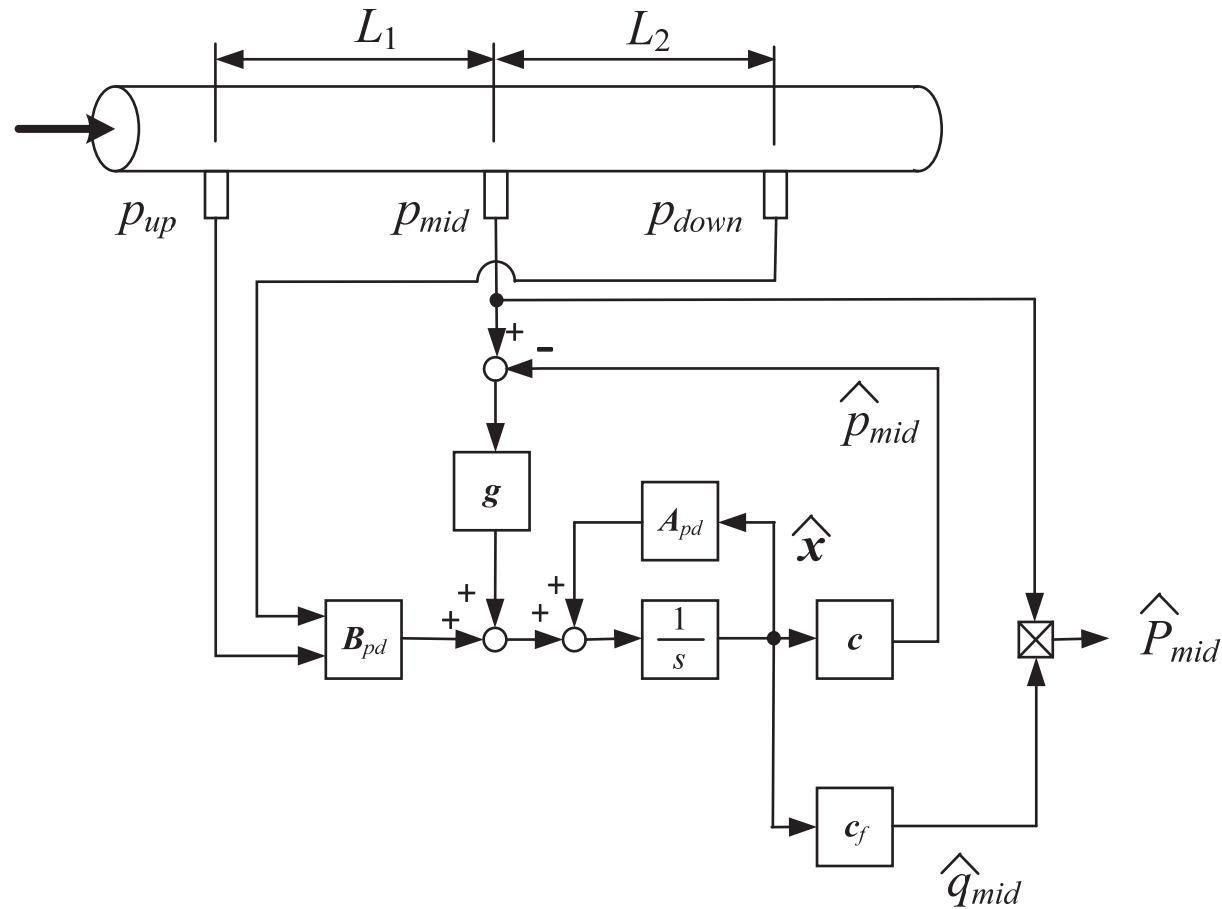
Posteriori estimation $\hat{\mathbf{x}}^-(k) = \mathbf{A}_{pd}\hat{\mathbf{x}}(k-1) + \mathbf{B}_{pd}\bar{\mathbf{p}}(k-1)$

Kalman gain $\mathbf{g} = \frac{\mathbf{P}\mathbf{c}}{\mathbf{c}^T\mathbf{P}\mathbf{c} + \sigma_w^2}$

Riccati equation $\mathbf{P} = \mathbf{A}_{pd} \left[\mathbf{P} - \frac{\mathbf{P}\mathbf{c}\mathbf{c}^T\mathbf{P}}{\mathbf{c}^T\mathbf{P}\mathbf{c} + \sigma_w^2} \right] \mathbf{A}_{pd}^T + \sigma_v^2 \mathbf{B}_{pd}\mathbf{B}_{pd}^T,$

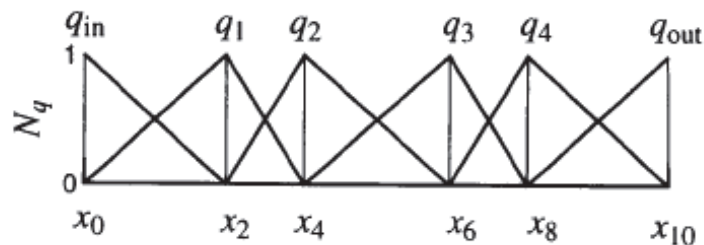
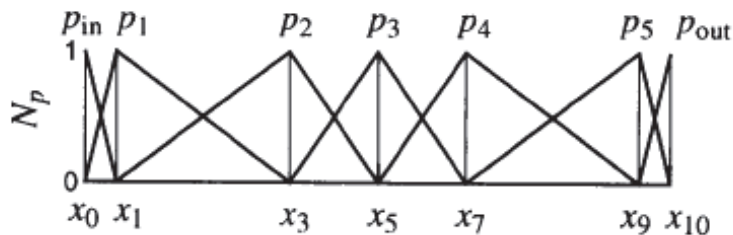
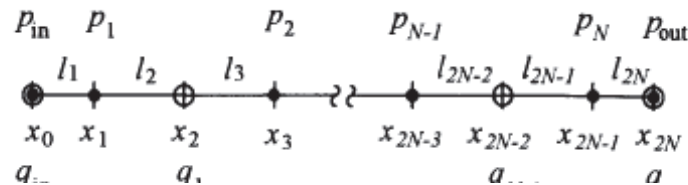
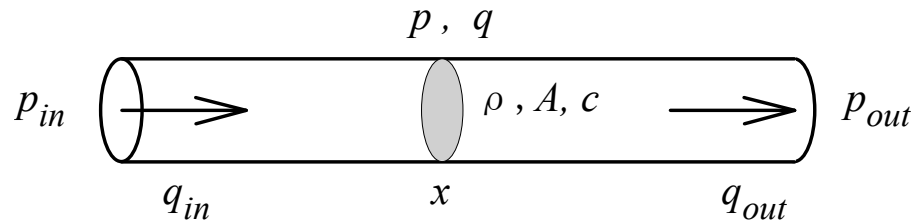
Variances $\sigma_w^2 = E(w^2), \text{ and } \sigma_v^2 = E(\mathbf{v}\mathbf{v}^T).$

2. Kalman filter theory



A measurement system using a Kalman filter

3. Pipeline mode; Optimized finite element model of pipeline dynamics



Interlacing grid system and linear shape function

Equation of motion

$$\frac{\partial q}{\partial t} + \frac{A}{\rho} \frac{\partial p}{\partial x} + p_f(q) = 0$$

Continuity equation

$$\frac{\partial p}{\partial t} + \frac{\rho c^2}{A} \frac{\partial q}{\partial x} = 0$$

Finite element approximation

$$\frac{dq}{dt} + \frac{A}{\rho} \mathbf{B}_{ofem} \mathbf{q} + \frac{A}{\rho} \mathbf{F}_{ofem} \bar{\mathbf{p}} + \mathbf{p}_f = 0$$

$$\frac{dp}{dt} + \frac{\rho c^2}{A} \mathbf{E}_{ofem} \mathbf{q} = 0$$

State variables at grid points

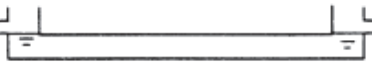
$$\mathbf{q} = [q_U, q_1, \dots, q_{N-1}, q_D]^T$$

$$\mathbf{p} = [p_1, p_2, \dots, p_N]^T$$

3. Pipeline model; Optimized finite element model of pipeline dynamics

The interlacing grid spacing is optimized to minimize the error function of model's eigenvalues compared with theoretical ones.

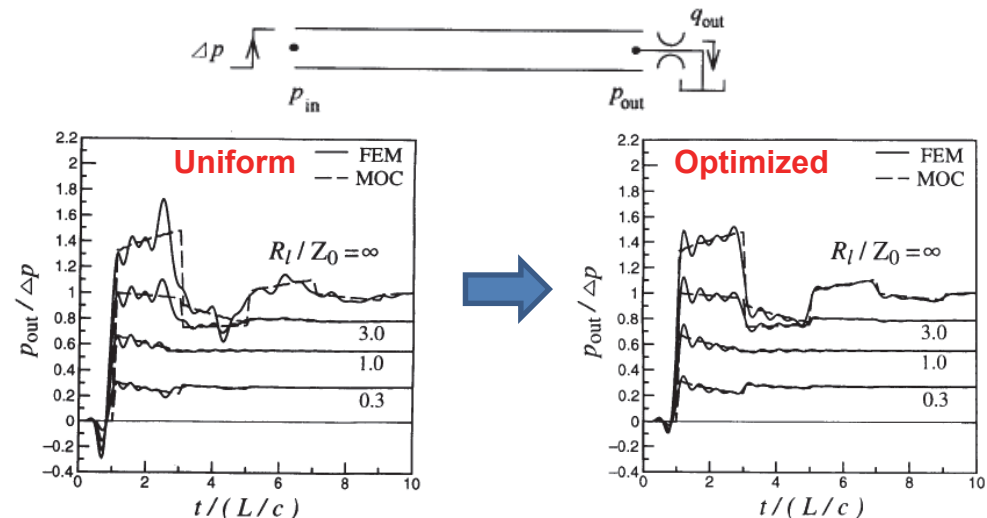
$$J(l_1, l_2, \dots, l_{N-1}) = \underbrace{\sum_{i=1}^{k_1} \left(\frac{\omega_{1i}}{2i\omega_n} - 1 \right)^2}_{\text{red}} + \underbrace{\sum_{i=1}^{k_2} \left(\frac{\omega_{2i}}{(2i-1)\omega_n} - 1 \right)^2}_{\text{blue}} + \underbrace{\sum_{i=1}^{k_3} \left(\frac{\omega_{3i}}{2(i-1)\omega_n} - 1 \right)^2}_{\text{green}}$$

$p_{in} = 0$  $p_{out} = 0$ $2i\omega_n$
 (1) Boundary condition 1

$p_{in} = 0$  $\frac{d}{dt}q_{out} = 0$ $(2i-1)\omega_n$
 (2) Boundary condition 2

$\frac{d}{dt}q_{in} = 0$  $\frac{d}{dt}q_{out} = 0$ $2(i-1)\omega_n$
 (3) Boundary condition 3

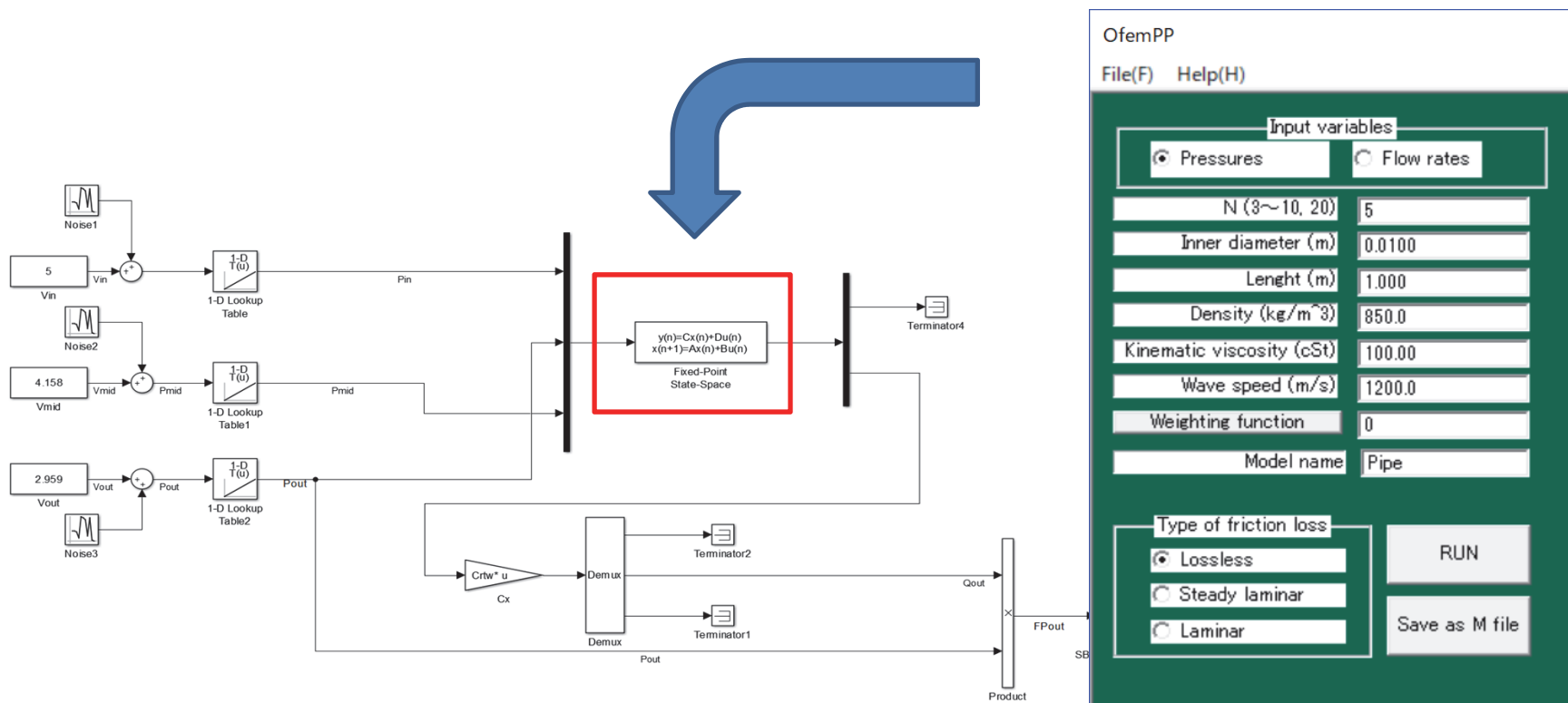
$\omega_n = \frac{\pi c}{2L}$



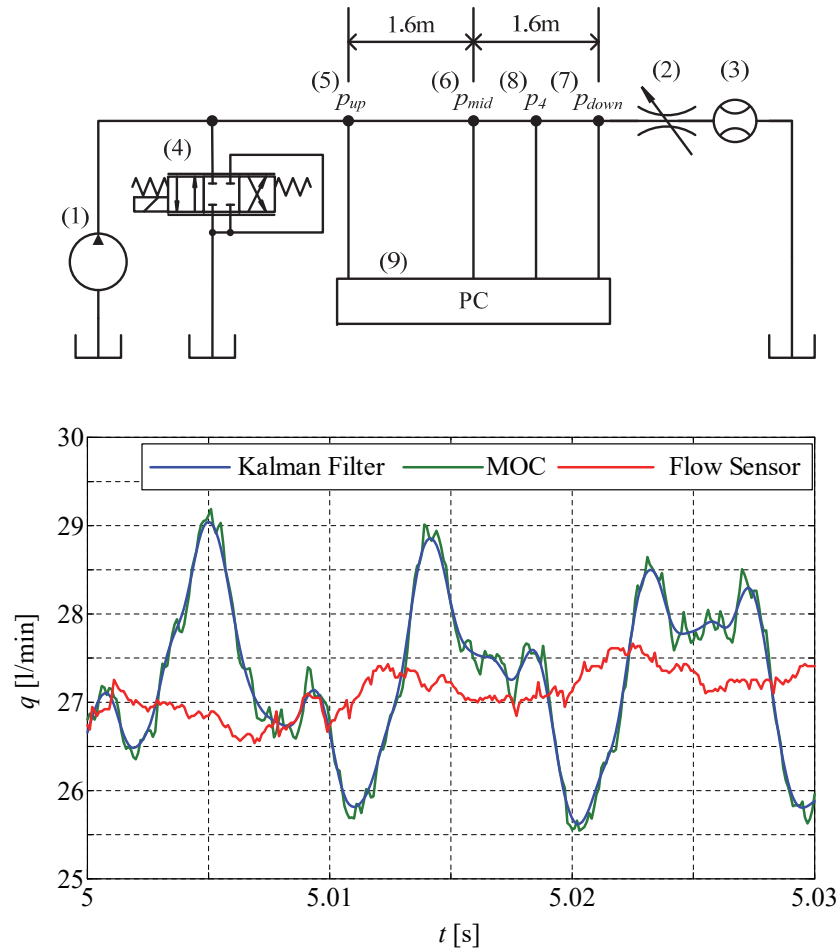
3. Pipeline model; Optimized finite element model of pipeline dynamics

Optimized finite element model can be used by a state space block of MATLAB/Simulink.

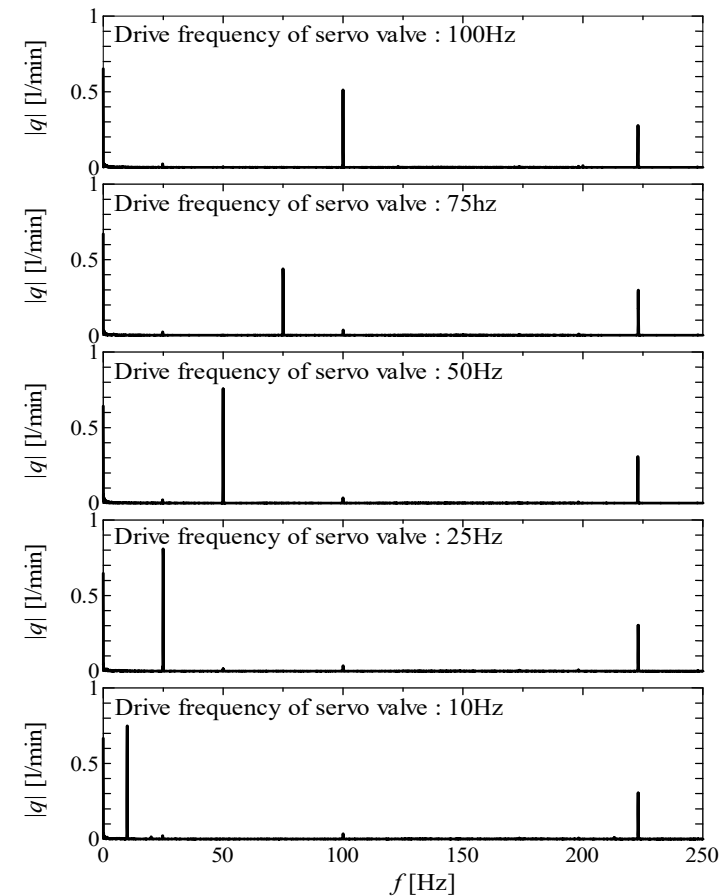
GUI for automatic calculation of state space representation



4. Off-line estimation of unsteady flow rate by the Kalman filter



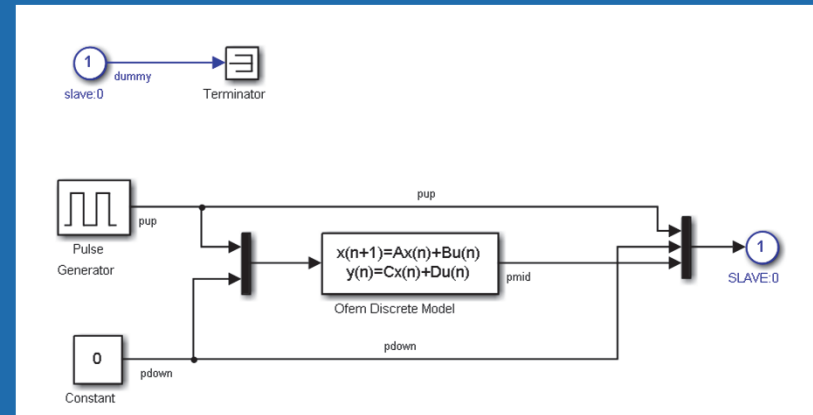
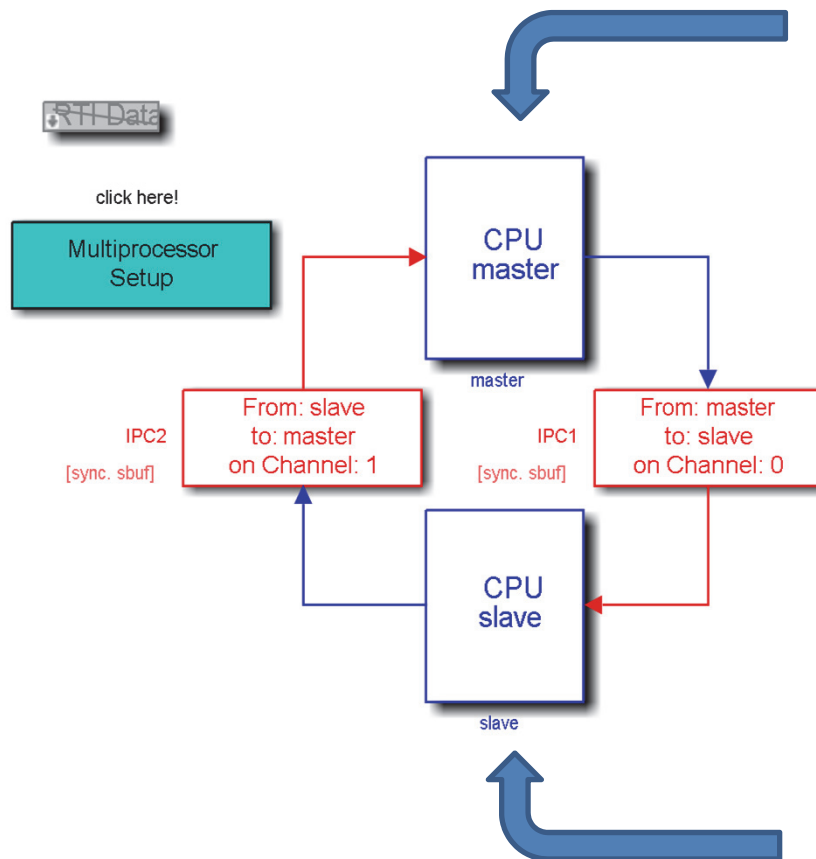
A test circuit of measuring unsteady flow rate



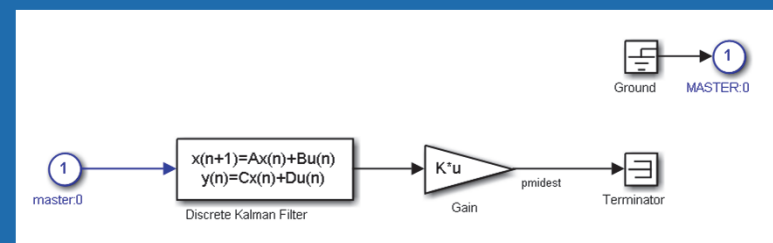
FFT analysis of unsteady flow rate estimated by the Kalman filter

5. Real-time implementation of Kalman filter

Kalman filter is installed in a real-time computing system.

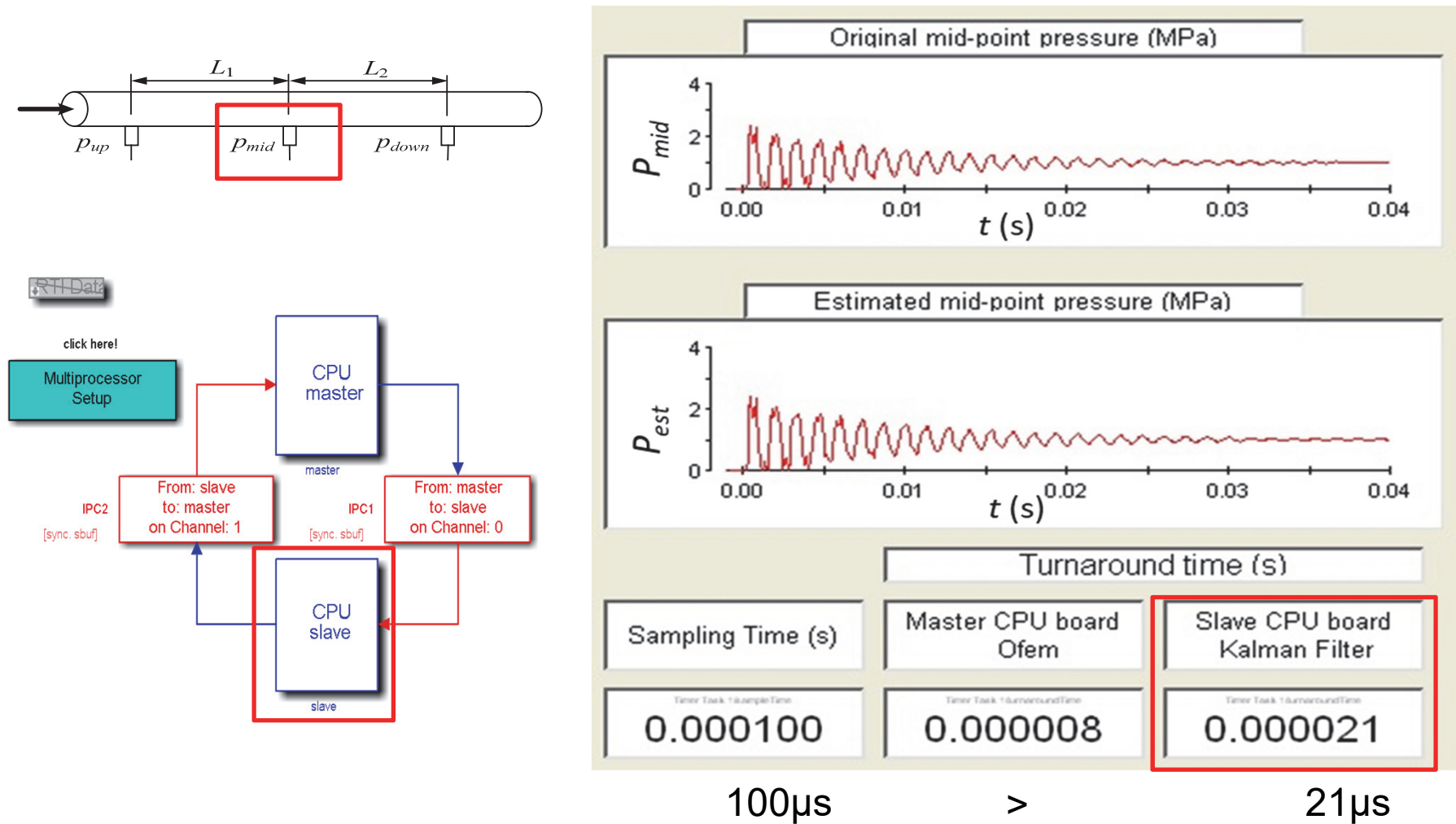


Target pipe simulator

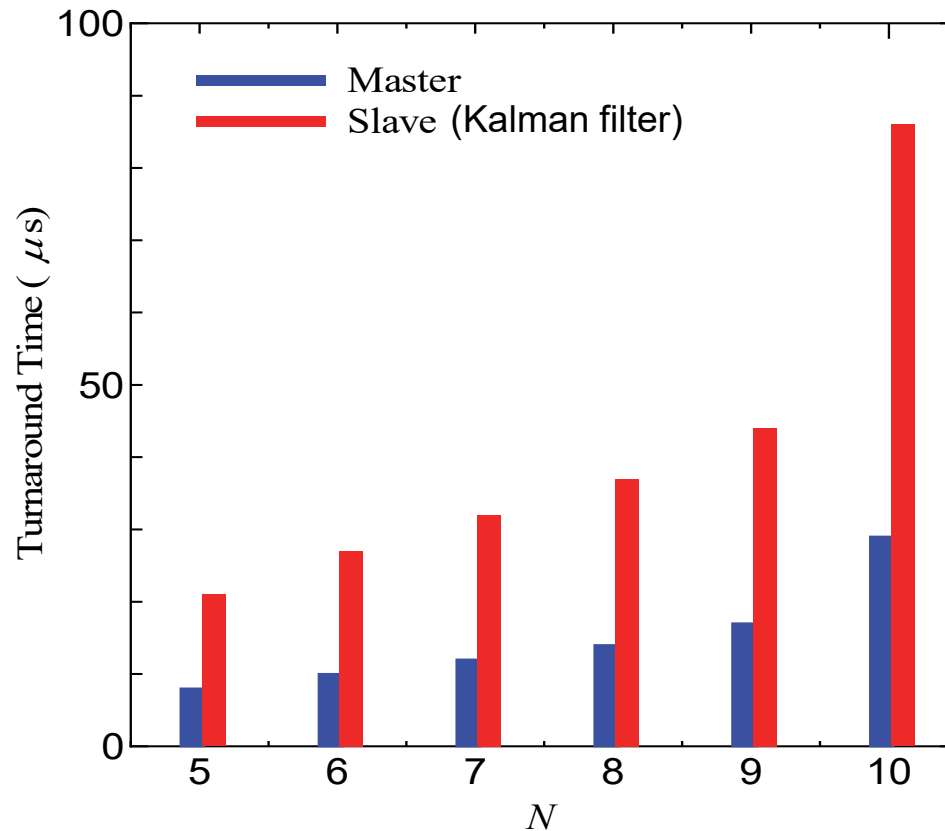


Kalman filter

5. Real-time implementation of Kalman filter



5. Real-time implementation of Kalman filter



CPU elapsed time depends on the number of finite elements of pipeline model.

Turnaround time for various numbers of elements N
(Sampling time: 100 μs for $N=9$ or less, 1000 μs for $N=10$)

6. Conclusion

- Real-time implementation of the Kalman filter is proposed to measure incompressible unsteady laminar flow rate and power of fluid flow in a pipe.
- A steady-state Kalman filter is implemented in a real-time computing system.
- It successfully works with a sampling time of 100 μ s.

Future works

- to reduce computational task
- to reduce the order of the pipeline model by order-reduction theory, etc.
- to select suitable number of finite elements

Acknowledgment

- This work is supported by Grant-in-Aid for Scientific Research (C) (JSPS KAKENHI Grant Number JP17K06226).

Thank you for your attention!

Contact:

- Kazushi SANADA
- Yokohama National University
- E-mail: sanada-kazushi-sn@ynu.ac.jp